VAPOUR-LIQUID EQUILIBRIUM IN THE ISOBUTYL FORMATE-ISOBUTYL ALCOHOL AND n-BUTYL FORMATE-ISOBUTYL ALCOHOL SYSTEMS AT ATMOSPHERIC PRESSURE*

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Dedicated to Professor E. Hala on the occasion of his 60th birthday.

Isobaric vapour-liquid equilibria in the isobutyl formate-isobutyl alcohol and n-butyl formate- - isobutyl alcohol systems have been measured at atmospheric pressure. A modified circulation still of the Gillespie type has been used for the measurements. The experimental data have been correlated by means of the third- and fourth-order Margules equations.

The knowledge of vapour-liquid equilibrium data in the alcohol-ester systems is required for the separation of mixtures produced by esterification of the alcohol with the acid. Since the title systems needed have not been found in the literature we have been made to carry out the experimental determination.

EXPERIMENTAL

Substances used. Isobutyl and n-butyl formates have been synthetized and purified in the Department of Heterogeneous Reactions of our Institute. Briefly, the raw product has been prepared by esterification of excess isobutyl alcohol (n-butyl alcohol) with formic acid in the presence of concentrated H_2SO_4 , then water has been distilled off azeotropically, the mixture has been neutralized and distilled. The excess of the alcohol in ester has been removed by boiling with acetic anhydride, the reaction mixture has been distilled, neutralized and finally the ester fraction has been thoroughly distilled on a packed column filled with the Dixon rings (\approx 40 TP). The purity of the fractions of the final ester has been checked during distillation by gas chromatography, the products being found not to contain either free alcohols or acids. The water content determined by the method of K. Fischer has been lower than 0·002%. The physico-chemical constants of the esters have been as follows: isobutyl formate, n.b.p. 98.54° C (ref.¹⁻³ 98.4), ¹²⁰ 0·8858 g/cm³ (ref.^{2,3} 0·88535), n²0 1·3854 (ref.^{1/–3} 1·38546); n-butyl formate, n.b.p. 107·32°C
ref.^{1,3} 106·6, ref.² 106·8), d²⁰ 0·9027 g/cm³ (ref.³ 0·8917), n2⁰ 1·3882 (ref.^{1,3} 1·38903). Isob

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Analytical method. The analysis of the equilibrium vapour and liquid samples has been made by means of a Paar digital densimeter DMA *OlC.* The dependence of the sample compositions on the measured value of period has been expressed by the relation

$$
(x_1M_1 + x_2M_2)/T = x_1M_1/T_1 + x_2M_2/T_2 + x_1x_2(x_1A_1 + x_2A_2 - x_1x_2A_3),
$$
\n(1)

where T is the measured value of oscillation period of mixture, M_1 and M_2 are molecular masses, T_1 and T_2 periods, $x_1, x_2 = 1 - x_1$ mole fractions of pure components 1 and 2, respectively, A_1 , A_2 , A_3 are constants evaluated from calibration measurements by the least-square method. Eq. (I) has represented the calibration data with mean deviation lower than 0.2%. In terms of the constants A_1 , A_2 , A_3 , the interpolation table has been computed (with a step $\Delta x = 0.001$) for direct reading of sample compositions.

Saturated vapour pressures of all three substances have been measured using a Swietoslawski ebulliometer⁶. The measured values of saturated vapour pressures of pure components have been correlated by the Antoine equation

$$
\log P^0 = A - B/(t + C), \qquad (2)
$$

where A, B, C are the adjustable parameters evaluated from the experimental data, P_{\sim}^{0} is the saturated vapour pressure (kPa) and t temperature ($\rm ^{o}C$).

Apparatus and procedure. The equilibrium measurements have been carried out in a modified Gillespie still. The description of the apparatus and measuring procedure can be found in the literature⁶. The pressure in the system has been maintained at 101.3 kPa by means of manostat and nitrogen overpressure and checked by measuring the boiling point of water in an ebullio-. meter connected parallel to the equilibrium still. The temperature has been measured by mercury- -in-glass calorimetric standard's calibrated by means of a Mueller bridge with a platinum resistance thermometer (Leeds and Northrup),'The equilibrium samples have been taken for analysis only when the boiling point in the still has not changed for 30 minutes.

RESULTS

The experimental values of saturated vapour pressures, the evaluated constants A, B, C of the Antoine equation (2) and the comparison of measured and calculated values are given in Tables I (isobutyl alcohol), II (n-butyl formate) and **III** (isobutyl formate).

The relations for the description of dependence of equilibrium variables in a binary system with non-ideal vapour phase can be written in the form

$$
\ln \gamma_1 = \ln (y_1 P / x_1 P_1^0) + ((B_{11} - V_1)(P - P_1^0) + P \delta_{12} y_2^2) / RT, \qquad (3a)
$$

$$
\ln \gamma_2 = \ln (y_2 P / x_2 P_2^0) + ((B_{22} - V_2) (P - P_2^0) + P \delta_{12} y_1^2) / R T, \qquad (3b)
$$

where

$$
\delta_{12} = 2B_{12} - B_{11} - B_{22}, \qquad (4)
$$

TABLE I Saturated Vapour Pressures of Isobutyl Alcohol

a Antoine vapour pressure constants: $A = 6.58646$, $B = 1322.416$, $C = 180.931$.

TABLE II

Saturated Vapour Pressures of n-Butyl Formate

^{*a*} Antoine vapour pressure constants: $A = 6.03014$, $B = 1245.850$, $C = 202.247$.

TABLE III Saturated Vapour Pressures of Isobutyl Formate

a Antoine vapour pressure constants; $A = 5.78268$, $B = 1093.134$, $C = 190.884$.

 γ_1 , γ_2 are the activity coefficients, y_1 , y_2 mole fractions in the vapour phase of the component 1 and 2, respectively, P is the system pressure, T the system absolute temperature, P_1^0 , P_2^0 are the saturated vapour pressures, V_1 , V_2 the molar volumes of liquid, B_{11} , B_{22} the second virial coefficients of pure components 1 and 2, B_{12} the second cross virial coefficient and *R* the gas constant.

The concentration dependence of activity coefficients has been expressed by means of the Margules 3rd order equation⁶

$$
\log(\gamma_1/\gamma_2) = x_2^2 A_{12} - x_1^2 A_{21} - 2x_1 x_2 (A_{12} - A_{21})
$$
 (5)

TABLE IV

Vapour-Liquid Equilibrium Data in the Isobutyl Formate(1)-Isobutyl Alcohol(2) System at 101'3 kPa

Constants of correlation equations: Marg. 3: $A_{12} = 0.2413$, $A_{21} = 0.2255$; Marg. 4: $A_{12} = 0.2331$, $A_{21} = 0.2155$, $D = -0.0640$; Second virial coefficients¹⁰: $B_{11} = -1171.00$, $B_{22} =$ $= -1230.00, B_{12} = -1187.00 \text{ cm}^3/\text{mol}.$

and the Margules 4th order equation⁶

$$
\log(\gamma_1/\gamma_2) = x_2^2 A_{12} - x_1^2 A_{21} - 2x_1 x_2 (A_{12} - A_{21} + (x_2 - x_1) D), \qquad (6)
$$

where A_{12} , A_{21} , D are constants characteristic of the given mixture and equation.

Since our aim has been to provide data for chemical engineers we have used the recommended⁷ objective function F suitable especially for the determination of the number of stages of distillation equipment, *viz.* the difference of the ratios of loga-

TABLE V

Vapour-Liquid Equilibrium Data in the n-Butyl Formate(l)- Isobutyl Alcohol(2) System at 101 '3 kPa

	x_1	y_1	$t, \degree C$	$(y_{1})_{\text{calc}} - y_{1})_{\text{exp}}^a$		
				Marg. 3	Marg. 4	
	0.0615	0.0912	106.96	-0.0035	0.0024	
	0.0830	0.1188	106.45	-0.0022	0.0022	
	0.0828	0.1205	$106 - 71$	-0.0043	0.0000	
	0.1112	0.1590	$106 - 34$	-0.0063	-0.0052	\sim
	0.1370	0.1910	$106 - 01$	-0.0064	-0.0089	
	0.1658	0.2267	105.65	-0.0081	-0.0146	
	0.2086	0.2698	105.22	-0.0034	-0.0153	
	0.2530	0.3158	104.86	-0.0032	-0.0189	
	0.3116	0.3688	104.54	0.0000	-0.0173	
	0.3712	0.4194	$104 - 29$	0.0021	-0.0132	
	0.4602	0.4830	104.22	0.0101	0.0031	
	0.5750	0.5772	104.28	0.0011	0.0077	
	0.7134	0.6955	$104 - 77$	-0.0149	-0.0002	
	0.7768	0.7564	105.08	-0.0244	-0.0118	
	0.8218	0.7944	$105 - 48$	-0.0223	-0.0135	
	0.8408	0.8096	105.65	-0.0193	-0.0125	
	0.8698	0.8394	105.84	-0.0192	-0.0161	
	0.9005	0.8642	106.23	-0.0095	-0.0102	
	0.9386	0.9072	106.61	-0.0040	-0.0083	
	0.9860	0.9678	$107 - 03$	0.0076	0.0046	
	Mean			0.0086	0.0093	

Constants of correlation equations: Marg. 3: $A_{12} = 0.1688$, $A_{21} = 0.2673$; Marg. 4: $A_{12} = 0.2470$, $A_{21} = 0.3303$, $D = 0.3531$; Second virial coefficients¹⁰: $B_{11} = -133300$, $B_{22} =$ $= -1168.00, B_{12} = -1230.00 \text{ cm}^3/\text{mol}.$

rithms of activity coefficients

$$
F = \ln(\gamma_1/\gamma_2)_{\text{exp}} - \ln(\gamma_1/\gamma_2)_{\text{calc}} \,. \tag{7}
$$

The constants of the correlation equations have been computed by least-square minimization of the function F.

Virial coefficients needed to compute activity coefficients in terms of Eqs (3) and (4) are very limited. Only second virial coefficients of isobutyl alcohol can be found in the literature⁸. For n-butyl formate even the critical constants are not known and have had to be estimated by means of the Lydersen method⁹. This has made us use the Hayden and O'Connell method¹⁰ for predicting the second virial coefficients of pure substances as well as for the mixtures. With regard to small differences in the boiling points of components in the binary systems and an approximate character of the estimated virial coefficients, the temperature dependence of the virial coefficients has not been considered and the values used have been computed for the temperature equal to the average value of normal boiling points of the respective pure components.

The results of the vapour-liquid equilibrium measurements together with the constants of correlation equations, second virial coefficients and the deviations between computed and experimental values of the vapour phase composition are given in Table IV (the isobutyl formate-isobutyl alcohol system) and Table V (the n-butyl formate-isobutyl alcohol system).

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